

# **DRAINAGE IMPACT ASSESSMENT REPORT**

**FOR**

**PROPOSED TEMPORARY WAREHOUSE (STORAGE OF CONSTRUCTION MATERIALS, METAL AND ELECTRONIC PARTS) AND OPEN STORAGE OF CONSTRUCTION MATERIALS FOR A PERIOD OF 3 YEARS**

**AT LOTS 130 (PART), 131, 132 (PART), 134(PART), 260(PART), 261(PART), 262, 263, 264 AND 268(PART) IN D.D.128 AND ADJOINING GOVERNMENT LAND, HA TSUEN, YUEN LONG, NEW TERRITORIES**

Date : February 2026

Report no. SDP/HT/001C

## Response to DSD's comment on 2<sup>nd</sup> December 2024

Item	DSD's comment	Response to comment
1	Please advise the location of the box culvert on the location plan, and advise the drainage flow path from the subject site to the public drainage system/streamcourse/sea/any recognized drainage facilities shown in the Lands Department's map in association with supporting site photos	The location of 1.5m dia. underground pipe and the drainage flow path from the subject site to the streamcourse is shown on the drainage plan. The site photo of the existing stream and 1.5m dia. underground pipe is appended in Appendix C.
2	Please provide photos of the box culvert to demonstrate the dimensions (including height) of the box culvert	The photo of the existing 1.5m dia. underground pipe is shown photo no. V6 and V7 as appended in Appendix C.
3	In the photo of the existing box culvert, it is noted that the box culvert is full of vegetation and therefore, the calculation could not reflect the actual condition.	The photo of the existing 1.5m dia. underground pipe is shown photo no. V6 and V7 as appended in Appendix C.
4	Please provide photos of the existing streamcourse at different sections to demonstrate the dimension of the streamcourse	The photos of the existing streamcourse is shown photo no. V1 to V5 as appended in Appendix C.
5	Please refer to DSD's Stormwater Drainage Manual (SDM) including SDM Corrigendum No. 1/2024 regarding rainfall intensity	The estimation of rainfall intensity is revised in accordance to SDM Corrigendum No. 1/2024 in this resubmission

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7. The Monitoring of Mitigation Measures
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## REFERENCES

1. Stormwater Drainage Manual, Planning Design and Management by DSD
2. Geotechnical Manual for Slopes by GEO
3. Standard Drawings by DSD

## 1. Introduction

This report presents the drainage impact assessment (DIA) to the existing drainage system outside the site from the proposed temporary warehouse (storage of construction materials, metal and electronic parts) and open storage of construction materials at lots 130 (part), 131, 132 (part), 134 (part), 260 (part), 261 (part), 262, 263, 264 and 268 (part) in D.D.128 and adjoining Government Land, Ha Tsuen, Yuen Long, New Territories.

The objective of the DIA report is to outline the catchment areas in the vicinity of the site, identifies and quantifies the potential drainage impact due to the proposed works and recommend the necessary mitigation measures to alleviate the impacts. The plan showing the the proposed surface channel and existing drainage system in the vicinity of the site is appended in **Appendix A**.

## 2. Design Parameters & Assumptions

The design criteria to be used for the modeling assessment are based on the standards set out in the Stormwater Drainage Manual, Fifth Edition (SDM). According to Section 6.6.1 of the SDM, the existing village drainage system in the vicinity of the development is classified as main rural catchment drainage system. Table 10 of the SDM recommends to be adopted a 50 years design return period storm event for the main rural drainage branch system.

### Stormwater Runoff (Q)

The rate of stormwater runoff used in this assessment report is estimated by the “Rational method” in which the peak runoff is calculated from the formula:

$$Q = K \times i \times A / 3600$$

where

Q	=	maximum runoff (L/s)
i	=	design mean intensity of rainfall (mm/hr)
A	=	area of catchment (m <sup>2</sup> )
K	=	runoff coefficient

### Time of Concentration (tc)

The time of concentration is defined as the time required for stormwater runoff to flow from the most remote part of the catchment area to the point in the drainage system under consideration. Based on the assumptions adopted in the Rational Method, this is the time taken for the peak runoff to become established at the considered section.

The time of concentration comprises the time for water flowing within natural catchments and along the man-made drainage pipes/channels. For natural catchments, the time of concentration is estimated by the modified form of the Brandsby William's equation.

$$t_o = \frac{0.14465L}{H^{0.2} A^{0.1}}$$

Where  $t_o$  = time of concentration of a natural catchment (min.)

A = catchment area (m<sup>2</sup>)

H = average slope (m per 100m), measured along the line of natural flow, from the summit of the catchment to the point under consideration

L = distance (on plan) measured on the line of natural flow between the summit and the point under consideration (m)

### Mean Rainfall Intensity (i)

Mean rainfall intensity-duration curves attached in this report are based on the Statistical analysis of long term rainfall records from the Hong Kong Observatory. A return period of 50 years is adopted.

### Runoff Coefficient (K)

The value of K is taken as 1 for developed paved area. For vegetated ground, the value of K is taken as 0.3.

## Calculation of flow capacity for Existing Stream and Box Culvert

Manning's Formula can be used to determine the capacity of the existing stream and box culvert

$$Q = K A R^{2/3} S^{1/2} \div n$$

Q = flow rate

A = cross sectional area of stream

R = hydraulic radius

S = slope of the stream

K = constant which is 1.49 for S.I. unit

n = surface roughness

### **3. Existing Drainage Condition**

A plan showing the existing catchments is enclosed in **Appendix A**. Currently, the surface runoff collected from the site is discharging to the existing 1.5m wide stream located at the west of the site and connected to existing 1.5m dia. pipe. As per the existing site condition, an additional peripheral U-channels area is considered necessary for the proposed development. A drainage proposal is required to be carried out for the proposed development.

### **4. Proposed Stormwater Drainage**

The proposed stormwater drainage works include surface U-channels at the peripheral of the site collecting the runoff from catchments within the site. The U-channels will connect and discharge the surface runoff to the existing stream located at the west of the site. Catchpits with 300mm sump are proposed at the discharged points of the proposed U-Channel to desilt the surface water before discharging to the drainage outside. The proposed stormwater drainage layout plan is shown in **Appendix A**.

## **5. Effect on Drainage Characteristics and Potential Drainage Impact from Proposed Works**

Since the proposed works only consist of the proposed temporary warehouse (storage of construction materials, metal and electronic parts) and open storage of construction materials, it is found that the proposed works would not obstruct the flow of the rain water run-off collected from the catchment areas to existing stream neither at its up-stream nor immediately down-stream. Besides, the catchment areas have no significant changes before and after the proposed works. It is considered the proposed works will not induce any adverse effect to the existing rain-water discharge system.

The capacity of the existing stream and 1.5m dia. pipe was checked and presented in **Appendix B**. Based on the assessment, it is found that the existing stream and 1.5mm dia. pipe have enough capacity to collect the run-off from its up-stream catchment area.

## **6. Mitigation Measures On The Existing Streamcourse During Construction Stage and Operation Stage**

A desilted catchpit would be proposed at the runoff's terminated discharge point prior to the discharging the runoff to the existing stream. The desilted catchpit would be constructed during the construction stage to prevent the sand / construction debris discharged into the existing stream during the construction works. Erosion protection measures such as discharge apron would be provided to the existing streamcourse at the outlet of proposed outfall.

## **7. The Monitoring of Mitigation Measures**

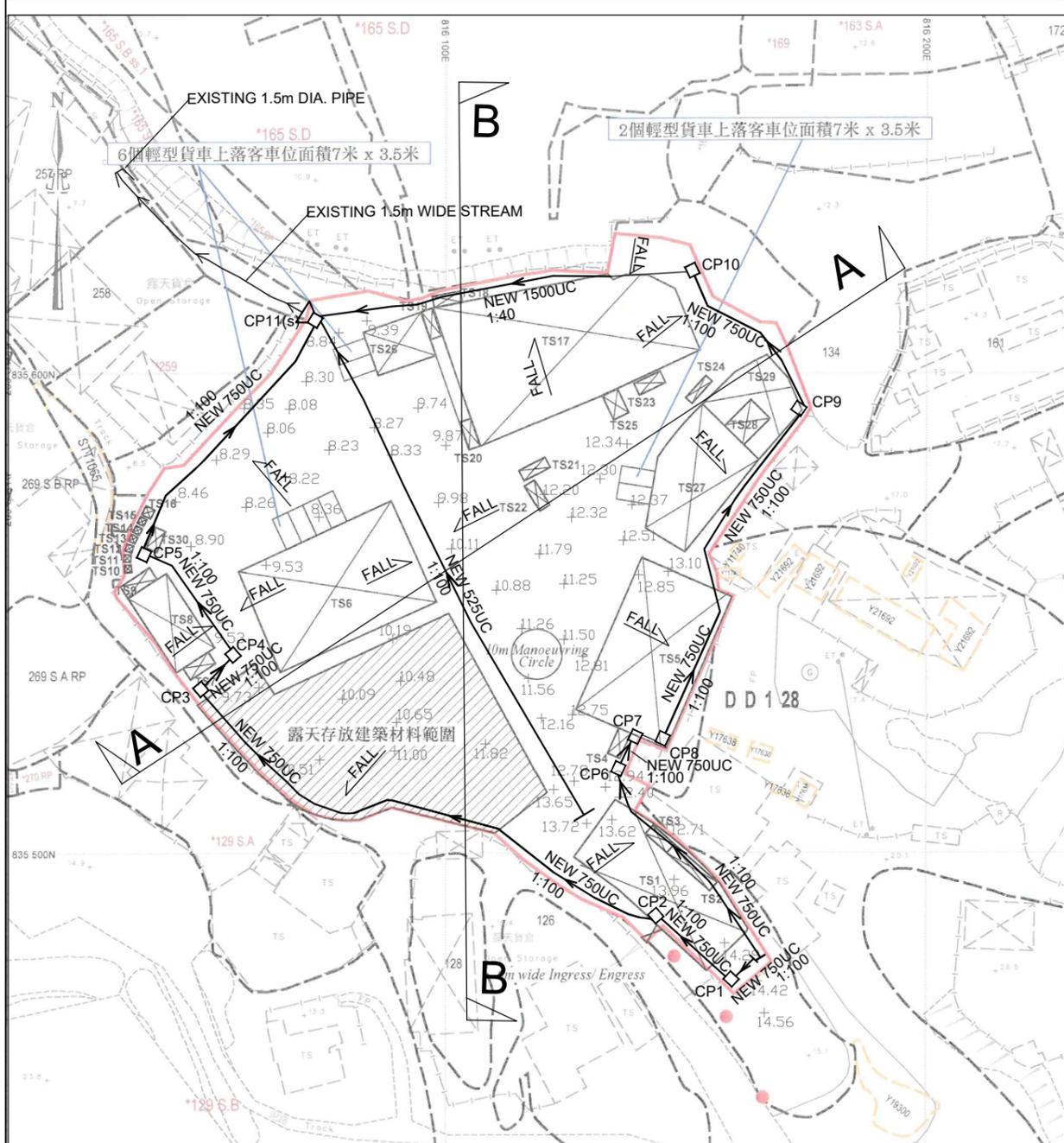
The proposed desilted catchpit would be regularly desilted by the applicant to prevent sand, silt, cementitious material or other objects from being washed down into the existing streamcourse.

## **8. Conclusion**

Based on the above discussion, it is considered that no potential drainage impact would be raised to the existing drainage system in the vicinity of the proposed works because the stream and 1.5m dia. pipe have enough capacity to collect the runoff from its up-stream catchment areas where the proposed works located. The proposed works are considered acceptable from the stormwater drainage point of view and will have no adverse effect on the drainage system outside

## **Appendix A**

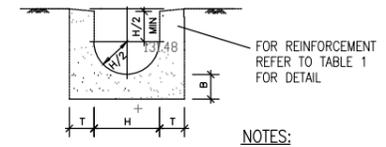
### **The Plan of the Proposed Works**



**LEGEND:**

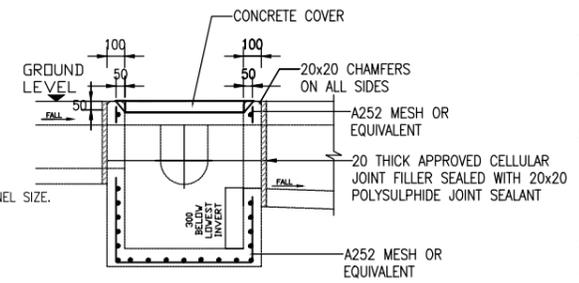
- +12.34 EXISTING GROUND LEVEL AT +12.34mPD
- 1:100 NEW 750UC PROPOSED 750mm U-CHANNEL WITH GRATING AT FALL 1: 100 (MIN)
- 1:100 NEW 525UC PROPOSED 525mm U-CHANNEL WITH GRATING AT FALL 1: 100 (MIN)

- CP11(s) □ PROPOSED COVERED DESILTED CATCHPIT NO. CP11
- CP1 □ PROPOSED COVERED CATCHPIT NO. CP1
- ◁ PROPOSED DISCHARGE APRON

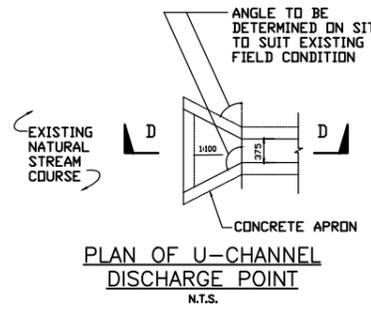


**U-CHANNEL**  
COMPLY WITH FIG 8.11 OF GEOTECHNICAL MANUAL FOR SLOPES

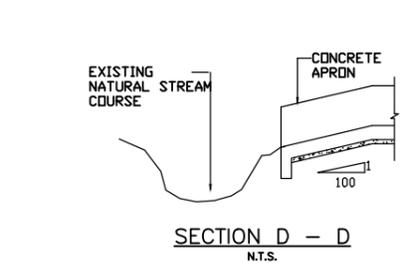
- CATCHPITS**
- ALL DIMENSIONS ARE IN MILLIMETRES
  - CONCRETE SURFACE FINISH SHALL BE CLASS U2 OR F3 AS APPROPRIATE



**SECTION D - D WITH DESILTED TRAP**  
COMPLY WITH CEDD'S DRAWING NO. DS C2405 AND C2406



**PLAN OF U-CHANNEL DISCHARGE POINT**  
N.T.S.



**SECTION D - D**  
N.T.S.

**GENERAL NOTE**

- THE PROPOSED DRAINAGE WORK, WHETHER WITHIN OR OUTSIDE THE LOT BOUNDARY, SHOULD BE CONSTRUCTED AND MAINTAINED BY THE LOT OWNER AT HIS OWN EXPENSE. FOR WORKS TO BE UNDERTAKEN OUTSIDE THE LOT BOUNDARY, PRIOR CONSENT AND AGREEMENT FROM DLO AND/OR RELEVANT PRIVATE LOT OWNER SHOULD BE SOUGHT.
- THE 100mm OPENING AT 1m C/C SHALL BE PROVIDED AT THE BOTTOM OF HOARDING OR WALLS IF ANY.

**CONCRETE STRENGTH AND STEEL REINFORCEMENT SPECIFICATION FOR DRAINAGE DETAILS**

- CONCRETE GRADE FOR CATCHPITS AND U-CHANNEL SHALL BE 30D DESIGN IN COMPLIANCE WITH CS1 : 2010 FOR BLINDING LAYER SHALL BE 15D, DESIGN COMPLY WITH CS1-2010.
- ALL MAIN BARS TO BE HOT ROLLED HIGH YIELD STEEL DEFORMED BAR COMPLY WITH CS2 : 2012  
Y - HIGH YIELD BAR 500 MPa  
M - MILD STEEL BAR 250 MPa
- CONCRETE COVER TO MAIN REINFORCEMENT TO BE 50mm.
- LAP LENGTH FOR ALL BARS TO BE 46x DIAMETER OF LARGER BAR TO BE LAPPED.
- REACTIVE ALKALI CONTENT EXPRESSED IN SODIUM OXIDE PER CUBIC METER OF CONCRETE SHOULD NOT EXCEED 3KG AS PER PNAP APP-74.

**HALF ROUND, U, AND STEPPED - CHANNELS**

- ALL DIMENSIONS ARE IN MILLIMETRES
- CONCRETE SURFACE FINISHING SHALL BE CLASS U2 OR F2 AS APPROPRIATE
- FOR HALF ROUND AND U - CHANNEL, SPACING OF EXPANSION JOINT IN CHANNELS, BERMS AND APRON TO BE 10m MAXIMUM. FOR STEPPED CHANNELS, EXPANSION JOINTS TO BE PROVIDED AT A MAXIMUM SPACING OF 10m.
- DIMENSIONS FOR HALF ROUND AND U-CHANNELS SEE TABLE 1.
- THE COVER FOR U-CHANNELS AND CATCHPIT SHALL COMPLY WITH CEDD'S STANDARD DRAWINGS NO. C2405 TO C2407 AND C2412.
- ALL PROPOSED U-CHANNELS SHALL BE COVERED WITH GRATING

**TABLE 1 : DIMENSION OF U-CHANNEL AND HALF-ROUND CHANNEL**

NORMAL SIZE H	T	B	REINFORCING
<300	100	100	NIL
375 - 675	150	150	NIL
750 - 900	175	175	A252 MESH PLACED CENTRALLY

**PROPOSED CATCHPIT SCHEDULE**

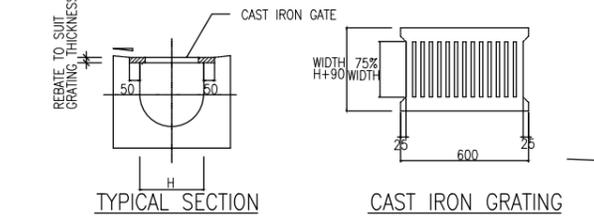
CATCHPIT NO.	C.L. (mPD)	I.L. (mPD)
CP1	14.29	13.44
CP2	13.96	13.11
CP3	9.73	8.88
CP4	9.73	8.80
CP5	8.90	8.05
CP6	12.94	12.09
CP7	12.94	12.02
CP8	12.94	11.97
CP9	12.37	11.20
CP10	12.30	10.70
CP11(s)	8.84	7.24

REV	DESCRIPTION	CHECKED	APPROVED	DATE
C	DSD'S COMMENT	RC	AY	RY FEB 26
B	DSD'S COMMENT	RC	AY	RY JULY 25
A	DSD'S COMMENT	RC	AY	RY AUG 24
	PLANNING SUBMISSION	RC	AY	RY JULY 24

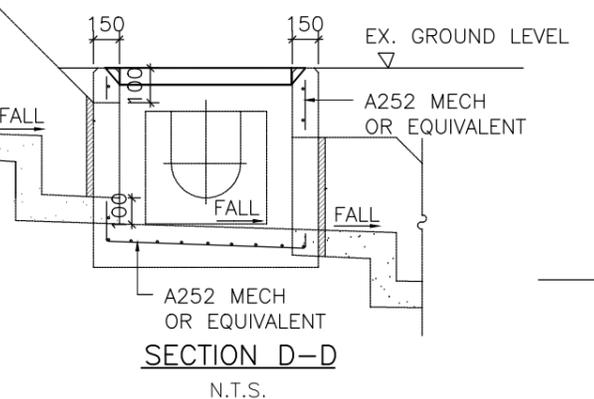
PROJECT TITLE:  
STORMWATER DRAINAGE PROPOSAL AT LOTS 130(PART) 131, 132(PART), 134(PART), 260(PART), 261(PART) 262, 263, 264 AND 268(PART) IN D.D.128  
HA TSUEN, YUEN LONG, NEW TERRITORIES

DRAWING TITLE:  
DRAINAGE PROPOSAL PLAN AND TYPICAL DETAILS

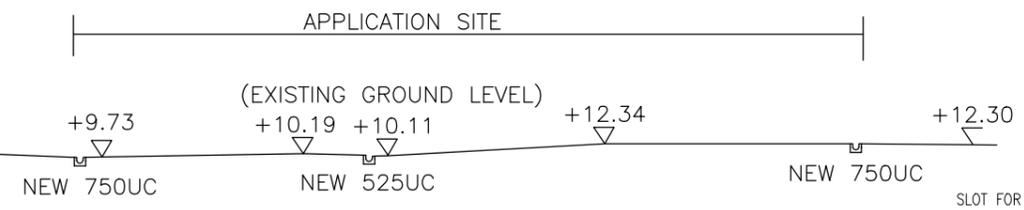
SCALE :	N.T.S.	CAD FILE:	CAD_REF
DRAWN	RY		
S.D	RC		
DESIGNED	RC		
CHECKED	AY		
		DRAWING NO.	SDP001C
		B.D. REF. NO.:	



**U-CHANNEL WITH CAST IRON GRATING**  
TYPICAL SECTION  
(DIMENSIONS ARE FOR GUIDANCE ONLY. CONTRACTOR MAY SUBMIT EQUIVALENT TYPE)

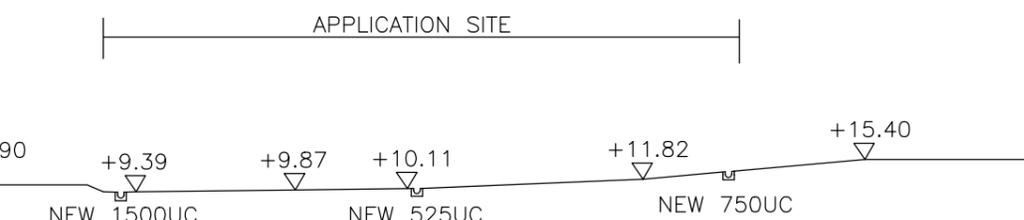


**SECTION D-D**  
N.T.S.



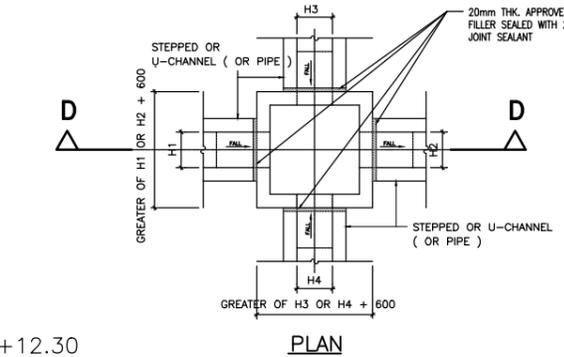
**SECTION A-A**

REMARKS : NO FILLING WORKS FOR THIS APPLICATION

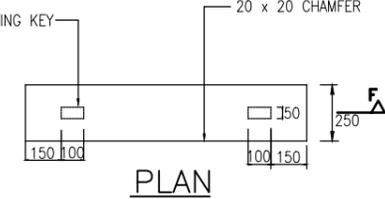


**SECTION B-B**

REMARKS : NO FILLING WORKS FOR THIS APPLICATION



**TYPICAL DETAILS OF CATCHPIT**



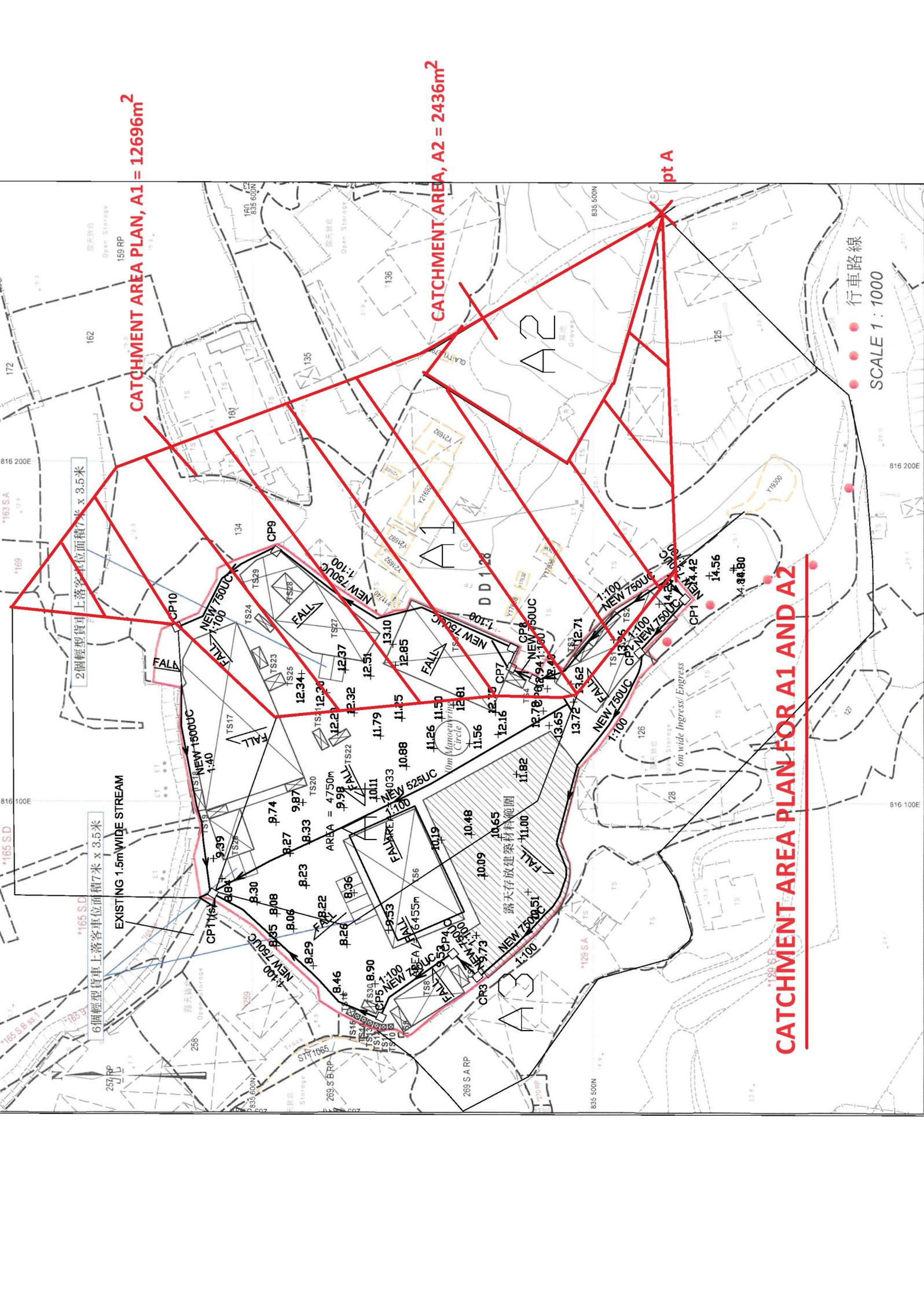
**PLAN**

N.T.S.  
GRADE 25D CONCRETE WITH ONE LAYER OF A 252 MESH REINFORCEMENT PLACED CENTRALLY F2 AND U2 FINISH

**PRECAST CONCRETE COVERS FOR CATCHPIT**  
N.T.S.

## **Appendix B**

### **Drainage Design of Proposed U-channel and Existing 1.5m Wide Stream & 1.5m Dia. Pipe**



CATCHMENT AREA PLAN, A1 = 12696m<sup>2</sup>

CATCHMENT AREA, A2 = 2436m<sup>2</sup>

CATCHMENT AREA PLAN FOR A1 AND A2

行車路線  
SCALE 1 : 1000

Drainage Design at lot 130, 131, 132,  
134, 260 to 264, 268 in DD128 Ha

Project No.: Tsuen, Yuen Long

Date: 12-Feb-26

Prepared by: Ray Cheng

Check for the drainage capacity of proposed 750UC

Catchment area,	A1	=	12696	m <sup>2</sup>	Assume k = 1.0 for paved surface
	A2	=	2436	m <sup>2</sup>	Assume k = 0.3 for unpaved surface
	Total Area, A	=	16696 + 0.3x2436		
		=	13426.8	m <sup>2</sup>	

Use Rational Method from Geo-Manual

$$Q = kiA/3600$$

where,

- Q = Maximum runoff (lit/sec)
- k = Runoff coefficient
- i = Design mean intensity of rainfall (mm/hr)
- A = Total catchment area (m<sup>2</sup>)

Longest distance from summit point to outlet, CP10	(Ld) =	310.00	m
Shortest distance from summit point to outlet, CP10	(Ls) =	183.00	m

Elevation of remote point (Pt A)	=	35.20	mPD
Elevation of outlet point, CP10	=	10.70	mPD

Average fall, H	=	$(z_1 - z_2) / L_s \times 100$	
	=	13.39	m per 100m

$$T_c = 0.14465 \times L_d / (H^{0.2} \times A^{0.1})$$

$$= 10.19 \text{ min}$$

Assume a 1 in 50 year design rainfall return period for rural area  
From SDM Corrigendum No. 1/2024

i	=	180	mm/hr	rainfall increase
Q	=	kiA/60	x 1.16	
		46725	lit/min	

From TGN 43A1

For proposed 750 UC with 1 in 100 gradient

Maximum capacity	=	74700	lit/min	>	46725	o.k.
The corresponding velocity	=	3.35	m/s	<	4	o.k.



Drainage Design at lot 130, 131, 132,  
134, 260 to 264, 268 in DD128 Ha

Project No.: Tsuen, Yuen Long  
Prepared by: Ray Cheng

Date: 12-Feb-26

Check for the drainage capacity of proposed 750UC

Catchment area, A3 = 12800 m<sup>2</sup> Assume k = 1.0 for paved surface

Use Rational Method from Geo-Manual

$$Q = kiA/3600$$

where,

Q = Maximum runoff (lit/sec)

k = Runoff coefficient

i = Design mean intensity of rainfall (mm/hr)

A = Total catchment area (m<sup>2</sup>)

Longest distance from summit point to outlet, CP11(s) (Ld) = 375.00 m

Shortest distance from summit point to outlet, CP11(s) (Ls) = 240.00 m

Elevation of remote point (Pt A) = 35.20 mPD

Elevation of outlet point, CP11(s) = 7.24 mPD

Average fall, H =  $(z_1 - z_2) / L_s \times 100$   
= 11.65 m per 100m

$T_c = 0.14465 \times L_d / (H^{0.2} \times A^{0.1})$   
= 12.89 min

Assume a 1 in 50 year design rainfall return period for rural area  
From SDM Corrigendum No. 1/2024

i = 175 mm/hr  
Q =  $kiA/60 \times 1.138$   
42485 lit/min

From TGN 43A1

For proposed 750 UC with 1 in 100 gradient

Maximum capacity = 74700 lit/min > 42485 o.k.

The corresponding velocity = 3.35 m/s < 4 o.k.

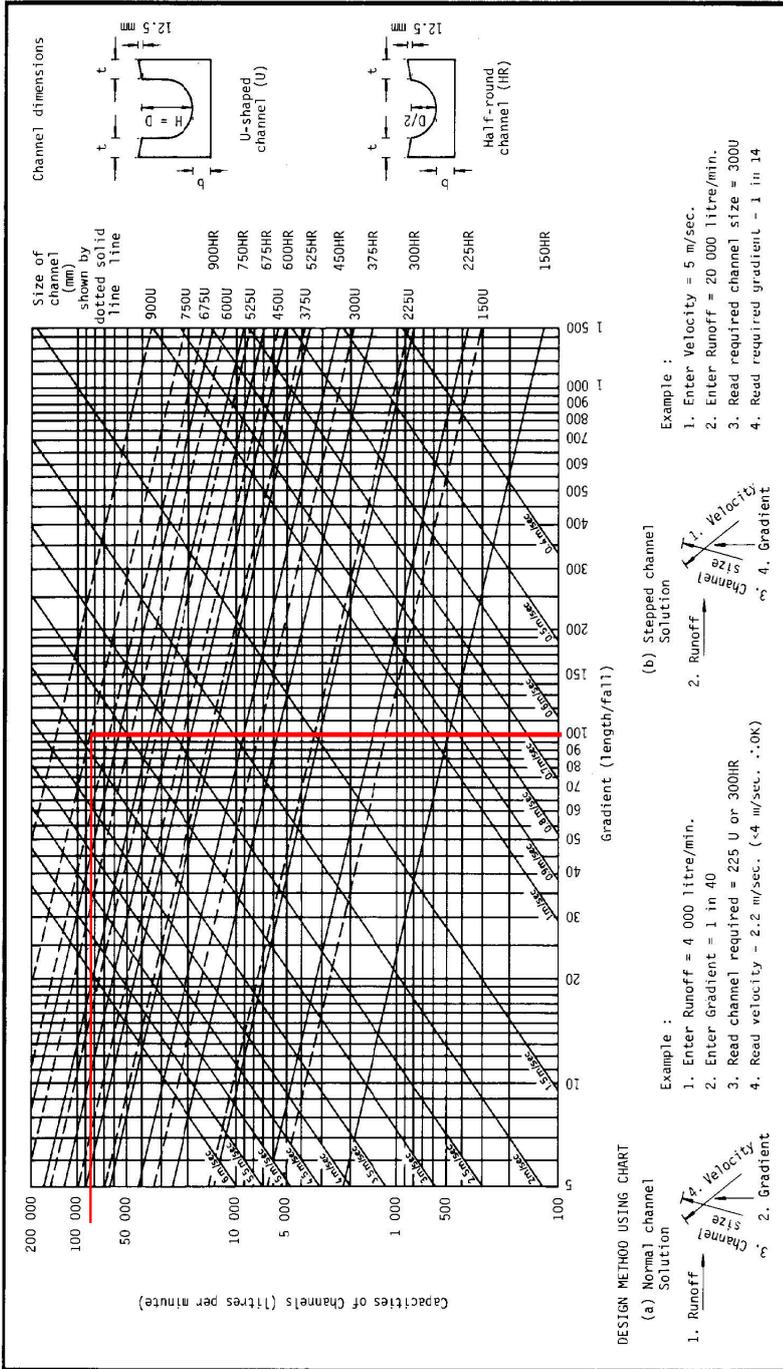


Figure 8.7 - Chart for the Rapid Design of Channels

Since 10% reduction would be considered for deposition of sediment, the capacity of the proposed 750UC should be  $83000 \times 0.9 = 74,700 \text{ lit/min}$ ,



Drainage Design at lot 130, 131, 132,  
134, 260 to 264, 268 in DD128 Ha

Project No.: Tsuen, Yuen Long

Date: 12-Feb-26

Prepared by: Ray Cheng

Check for the drainage capacity of proposed 525UC

Catchment area, A4 = 4033 m<sup>2</sup> Assume k = 1.0 for paved surface

Use Rational Method from Geo-Manual

$$Q = kiA/3600$$

where,

Q = Maximum runoff (lit/sec)

k = Runoff coefficient

i = Design mean intensity of rainfall (mm/hr)

A = Total catchment area (m<sup>2</sup>)

Longest distance from summit point to outlet, CP11(s)

(Ld) = 137.00 m

Shortest distance from summit point to outlet, CP11(s)

(Ls) = 120.00 m

Elevation of remote point (Pt C) =

13.72 mPD

Elevation of outlet point, CP11(s) =

7.24 mPD

Average fall, H =

$$(z_1 - z_2) / L_s \times 100$$

= 5.40 m per 100m

$$T_c = 0.14465 \times L_d / (H^{0.2} \times A^{0.1})$$

= 6.17 min

Assume a 1 in 50 year design rainfall return period for rural area

From SDM Corrigendum No. 1/2024

i = 205 mm/hr

Q =  $\frac{kiA}{60} \times 1.138$   
15681 lit/min

From TGN 43A1

For proposed 525 UC with 1 in 100 gradient

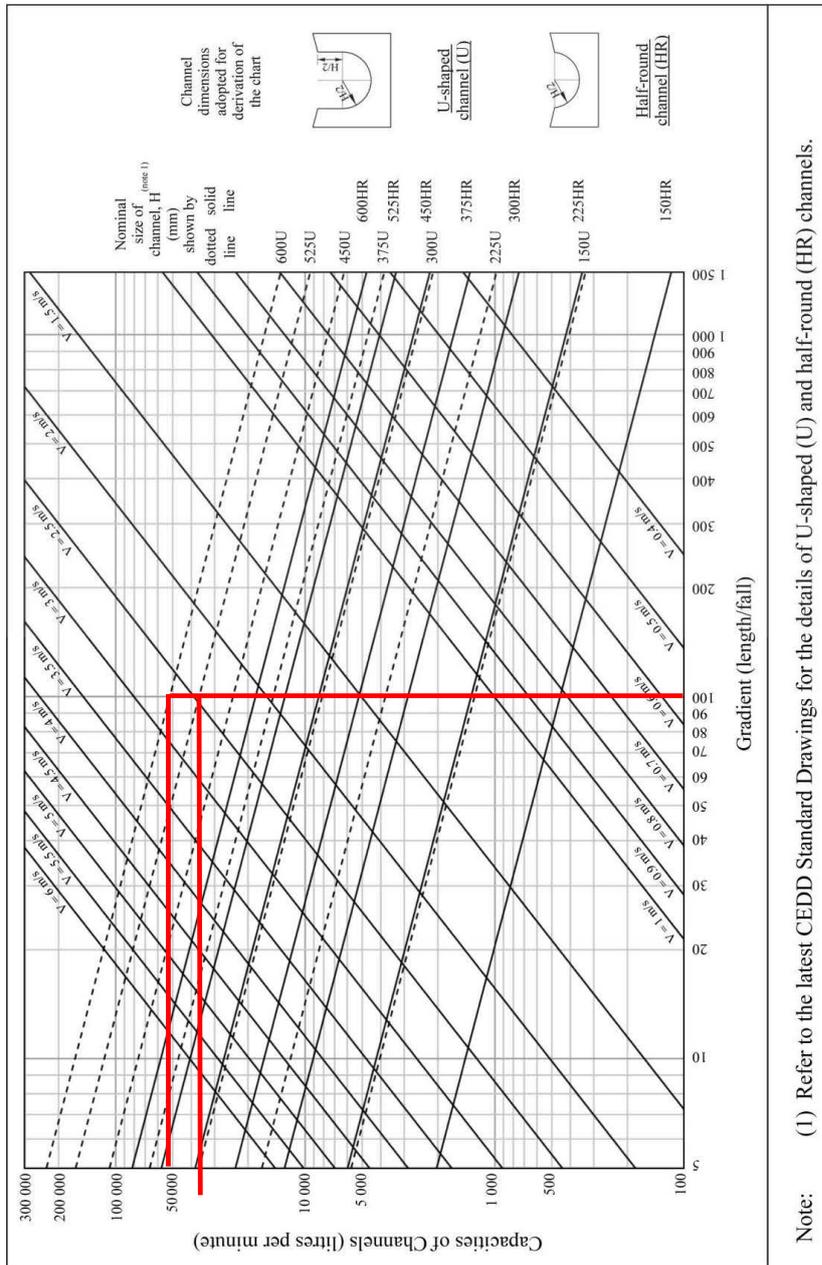
Maximum capacity = 32400 lit/min > 15681 o.k.

The corresponding velocity = 2.50 m/s < 4 o.k.

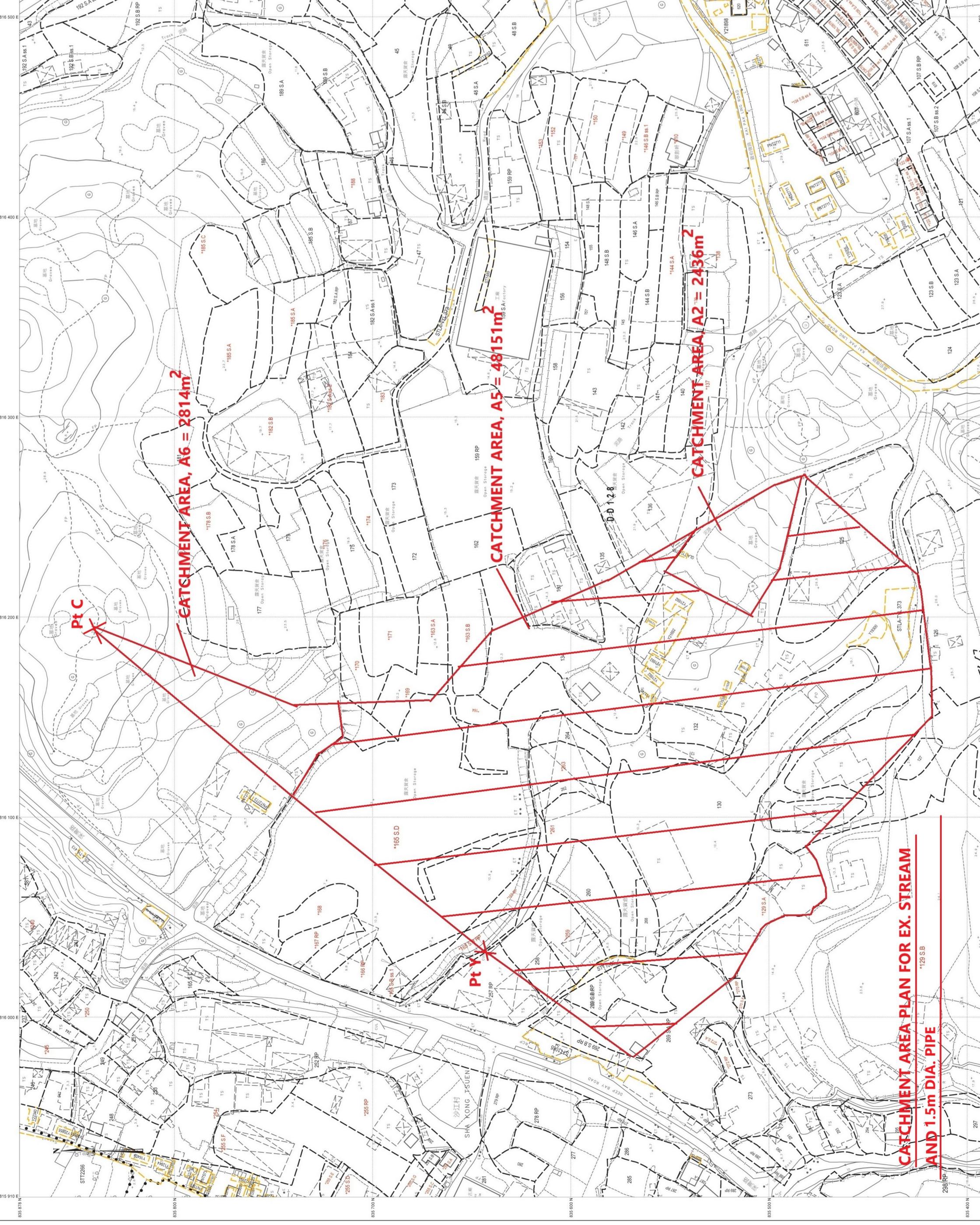
**GEO Technical Guidance Note No. 43 (TGN 43)**  
**Guidelines on Hydraulic Design of U-shaped and Half-round Channels on Slopes**

Issue No.: 1      Revision: -      Date: 05.06.2014      Page: 3 of 3

Figure 1 - Chart for the rapid design of U-shaped and half-round channels up to 600 mm



**Since 10% reduction would be considered for deposition of sediment, the capacity of the proposed 525UC should be 36000 x 0.9 = 32,400 lit./min,**



Pt C

CATCHMENT AREA, A6 = 2814m<sup>2</sup>

CATCHMENT AREA, A5 = 48151m<sup>2</sup>

CATCHMENT AREA, A2 = 2436m<sup>2</sup>

Pt Y

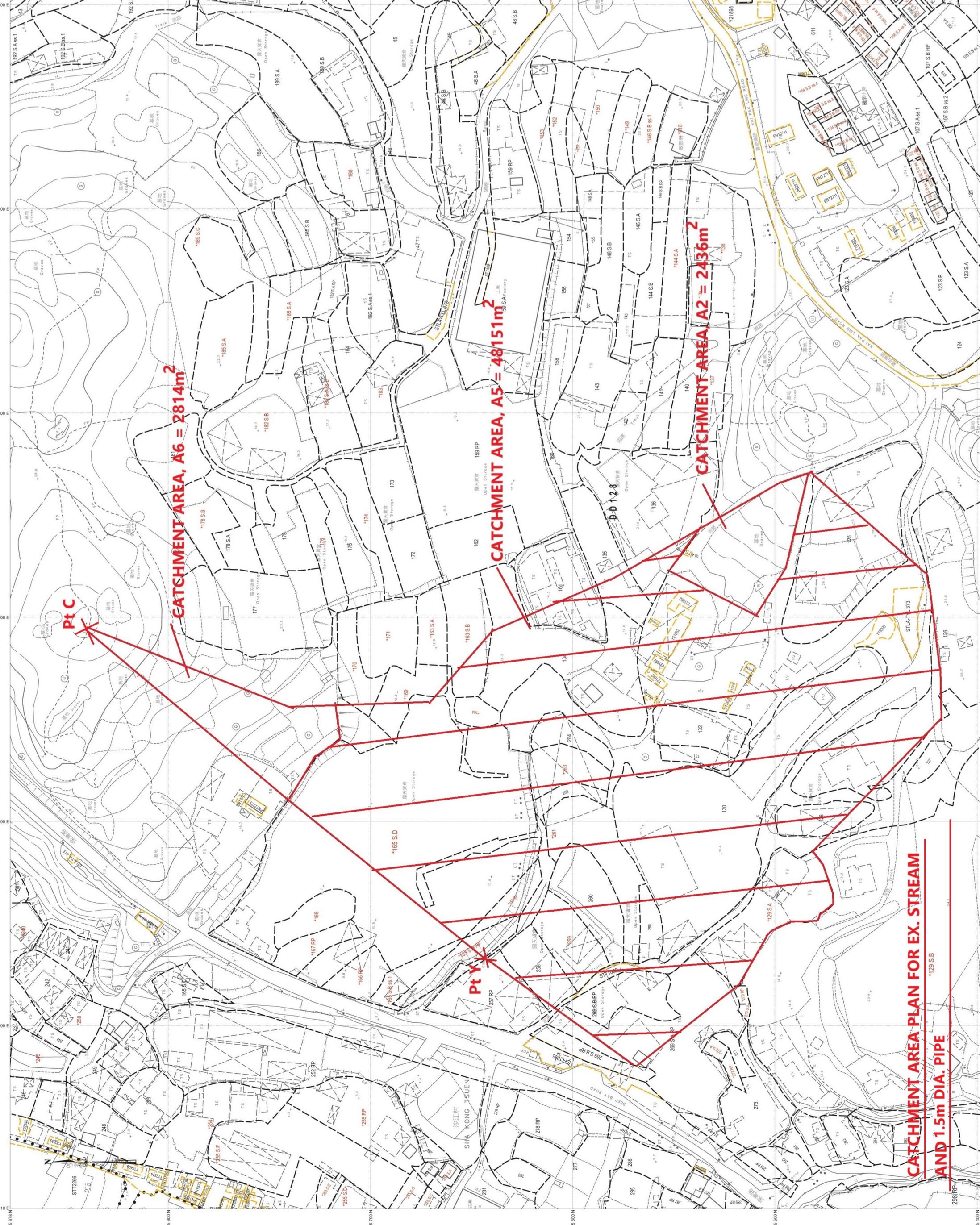
CATCHMENT AREA PLAN FOR EX. STREAM

AND 1.5m DIA. PIPE

SHA KONG TSUEN

DEEP BAY ROAD

KAI PAK LING ROAD



Drainage Design at lot 130, 131, 132,  
134, 260 to 264, 268 in DD128 Ha

Project No.: Tsuen, Yuen Long Date: 12-Feb-26  
Prepared by: Ray Cheng

Check for the drainage capacity of existing stream and 1.5m dia. pipe

Catchment area,	A5	=	48151	m <sup>2</sup>	Assume k = 1.0 for paved surface
	A2	=	2436	m <sup>2</sup>	Assume k = 0.3 for unpaved surface
	A6	=	2814		
	Total Area, A	=	48151 + 0.3x(2436+2814)		
		=	49726	m <sup>2</sup>	

Use Rational Method from Geo-Manual

$Q = kiA/3600$  where,

Q = Maximum runoff (lit/sec)  
k = Runoff coefficient  
i = Design mean intensity of rainfall (mm/hr)  
A = Total catchment area (m<sup>2</sup>)

Longest distance from summit point to outlet, Pt Y (Ld) = 400.00 m  
Shortest distance from summit point to outlet, Pt Y (Ls) = 255.00 m

Elevation of remote point (Pt C) = 36.50 mPD  
Elevation of outlet point, Pt Y = 7.24 mPD

Average fall, H =  $(z_1 - z_2) / L_s \times 100$   
= 11.47 m per 100m

$T_c = 0.14465 \times L_d / (H^{0.2} \times A^{0.1})$   
= 12.02 min

Assume a 1 in 50 year design rainfall return period for rural area  
From SDM Corrigendum No. 1/2024

i = 180 mm/hr  
Q =  $kiA/60 \times 1.138$   
169765 lit/min

# Drainage Design and Checking

Page no.

Project No.:  
Prepared by:

Ray Cheng

Date: 12-Feb-26

## Check for the drainage capacity (Existing 1.5m wide and 1.5m depth Stream course)

From Manning Equation, for existing 1.5m width and 1.5m depth streamcourse

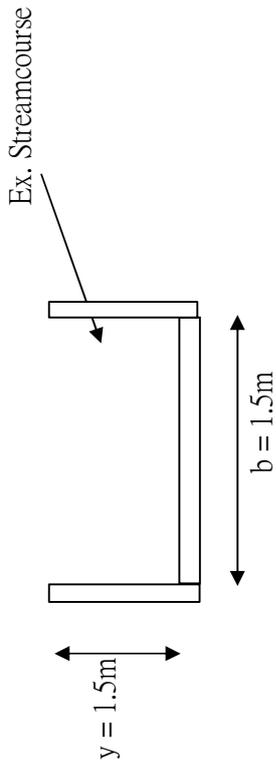
$$\text{Max. capacity of streamcourse, } Q = \frac{k(R^{2/3})(S^{1/2})}{n} A$$

$$R = A/P \text{ and } P = b + 2y$$

$$R = 0.50 \quad k = 1$$
$$S = 0.025 \quad n = 0.04$$

$$Q = 268935 \quad \text{lit/min} \quad > 169765 \text{ lit/min}$$

O.K.



ie hydraulic gradient = velocities in m/s **The capacity of 1.5m dia. pipe = 7.578x1000x60**  
 1 in 333 to 1 in 13 discharges in m<sup>3</sup>/s = **454,680 l/min > 169,765 l/min**

Gradient	Pipe diameters in mm.											
	900	975	1000	1050	1100	1200	1350	1500	1650	1800	1950	2100
0.00300 1/ 333	1.709	1.796	1.824	1.880	1.935	2.042	2.195	2.342	2.483	2.619	2.750	2.877
	1.087	1.341	1.433	1.628	1.839	2.309	3.142	4.139	5.309	6.663	8.212	9.963
0.00320 1/ 313	1.765	1.855	1.885	1.942	1.999	2.109	2.268	2.419	2.565	2.705	2.840	2.971
	1.123	1.385	1.480	1.682	1.900	2.385	3.246	4.275	5.484	6.883	8.482	10.292
0.00340 1/ 294	1.820	1.913	1.943	2.003	2.061	2.175	2.338	2.494	2.644	2.789	2.928	3.063
	1.158	1.428	1.526	1.734	1.959	2.459	3.347	4.408	5.654	7.096	8.745	10.610
0.00360 1/ 278	1.873	1.969	2.000	2.061	2.121	2.238	2.406	2.567	2.721	2.870	3.013	3.153
	1.192	1.470	1.571	1.785	2.016	2.531	3.444	4.536	5.819	7.303	9.000	10.919
0.00380 1/ 263	1.925	2.023	2.055	2.118	2.180	2.300	2.473	2.638	2.796	2.949	3.096	3.239
	1.225	1.510	1.614	1.834	2.071	2.601	3.539	4.661	5.979	7.504	9.247	11.220
0.00400 1/ 250	1.975	2.076	2.109	2.173	2.237	2.360	2.537	2.707	2.869	3.026	3.177	3.324
	1.257	1.550	1.656	1.882	2.126	2.669	3.632	4.783	6.135	7.700	9.489	11.513
0.00420 1/ 238	2.025	2.127	2.161	2.227	2.292	2.419	2.600	2.774	2.940	3.101	3.256	3.406
	1.286	1.588	1.697	1.929	2.178	2.735	3.722	4.902	6.287	7.891	9.724	11.798
0.00440 1/ 227	2.072	2.178	2.212	2.280	2.346	2.476	2.662	2.839	3.010	3.174	3.333	3.487
	1.318	1.626	1.738	1.974	2.230	2.800	3.810	5.018	6.436	8.078	9.954	12.077
0.00460 1/ 217	2.119	2.227	2.262	2.332	2.400	2.532	2.722	2.904	3.078	3.246	3.408	3.566
	1.348	1.663	1.777	2.019	2.280	2.863	3.896	5.131	6.582	8.260	10.179	12.350
0.00480 1/ 208	2.165	2.275	2.311	2.382	2.451	2.587	2.781	2.966	3.145	3.316	3.482	3.643
	1.378	1.699	1.815	2.063	2.330	2.925	3.980	5.242	6.724	8.438	10.399	12.616
0.00500 1/ 200	2.210	2.323	2.359	2.431	2.502	2.640	2.838	3.028	3.210	3.385	3.554	3.718
	1.406	1.734	1.853	2.105	2.378	2.986	4.063	5.351	6.863	8.613	10.614	12.877
0.00550 1/ 182	2.319	2.437	2.475	2.551	2.625	2.770	2.978	3.176	3.367	3.551	3.728	3.900
	1.475	1.819	1.944	2.209	2.495	3.132	4.262	5.613	7.200	9.035	11.134	13.509
0.00600 1/ 167	2.423	2.546	2.586	2.665	2.743	2.894	3.111	3.318	3.517	3.709	3.895	4.074
	1.541	1.901	2.031	2.308	2.606	3.273	4.453	5.864	7.521	9.439	11.631	14.111
0.00650 1/ 154	2.522	2.650	2.692	2.774	2.855	3.012	3.238	3.454	3.662	3.861	4.054	4.241
	1.604	2.079	2.214	2.502	2.793	3.407	4.635	6.104	7.829	9.826	12.108	14.690
0.00700 1/ 143	2.618	2.751	2.794	2.880	2.963	3.127	3.361	3.585	3.800	4.008	4.208	4.402
	1.665	2.054	2.195	2.493	2.806	3.536	4.811	6.336	8.126	10.198	12.567	15.246
0.00750 1/ 133	2.710	2.848	2.893	2.981	3.068	3.237	3.480	3.712	3.934	4.149	4.356	4.557
	1.724	2.126	2.272	2.581	2.916	3.661	4.981	6.559	8.413	10.557	13.009	15.783
0.00800 1/ 125	2.800	2.942	2.988	3.079	3.169	3.343	3.594	3.834	4.064	4.285	4.499	4.707
	1.781	2.196	2.347	2.667	3.012	3.781	5.145	6.775	8.689	10.905	13.437	16.302
0.00850 1/ 118	2.886	3.033	3.081	3.175	3.267	3.447	3.705	3.952	4.189	4.418	4.638	4.852
	1.836	2.264	2.419	2.749	3.105	3.898	5.304	6.984	8.958	11.242	13.852	16.806
0.00900 1/ 111	2.970	3.121	3.170	3.267	3.362	3.547	3.813	4.067	4.311	4.546	4.773	4.993
	1.890	2.330	2.490	2.829	3.195	4.012	5.458	7.188	9.219	11.569	14.255	17.295
0.00950 1/ 105	3.052	3.207	3.258	3.357	3.455	3.645	3.918	4.179	4.430	4.671	4.904	5.130
	1.942	2.394	2.558	2.907	3.283	4.122	5.608	7.385	9.472	11.887	14.647	17.770
0.01000 1/ 100	3.132	3.291	3.343	3.445	3.545	3.740	4.020	4.288	4.545	4.793	5.032	5.264
	1.992	2.457	2.625	2.983	3.369	4.230	5.754	7.578	9.710	12.107	15.029	18.233
0.01100 1/ 91	3.285	3.452	3.506	3.614	3.719	3.923	4.217	4.498	4.768	5.028	5.279	5.522
	2.080	2.557	2.726	3.109	3.514	4.437	6.036	7.949	10.195	12.704	15.764	19.121

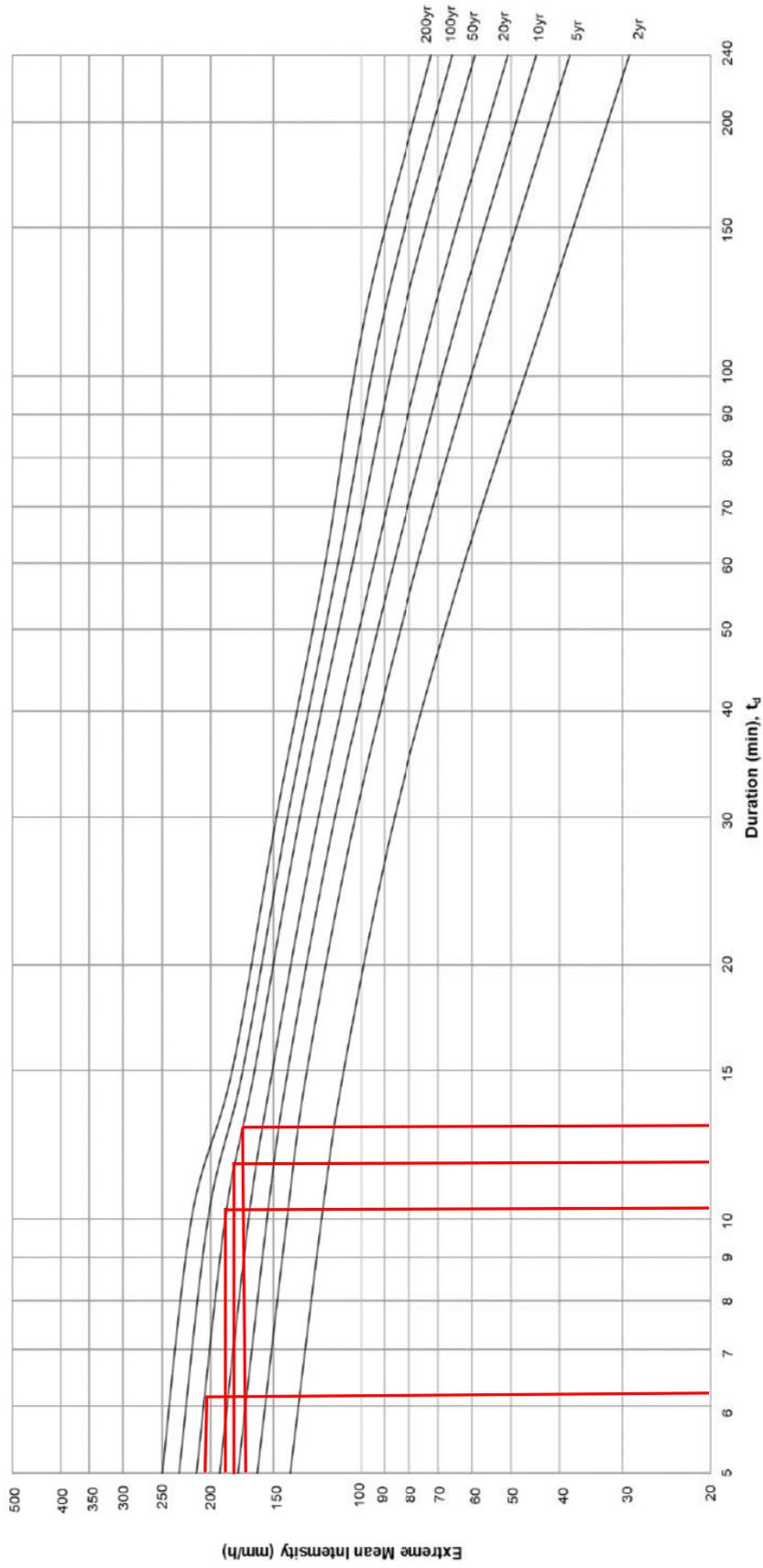
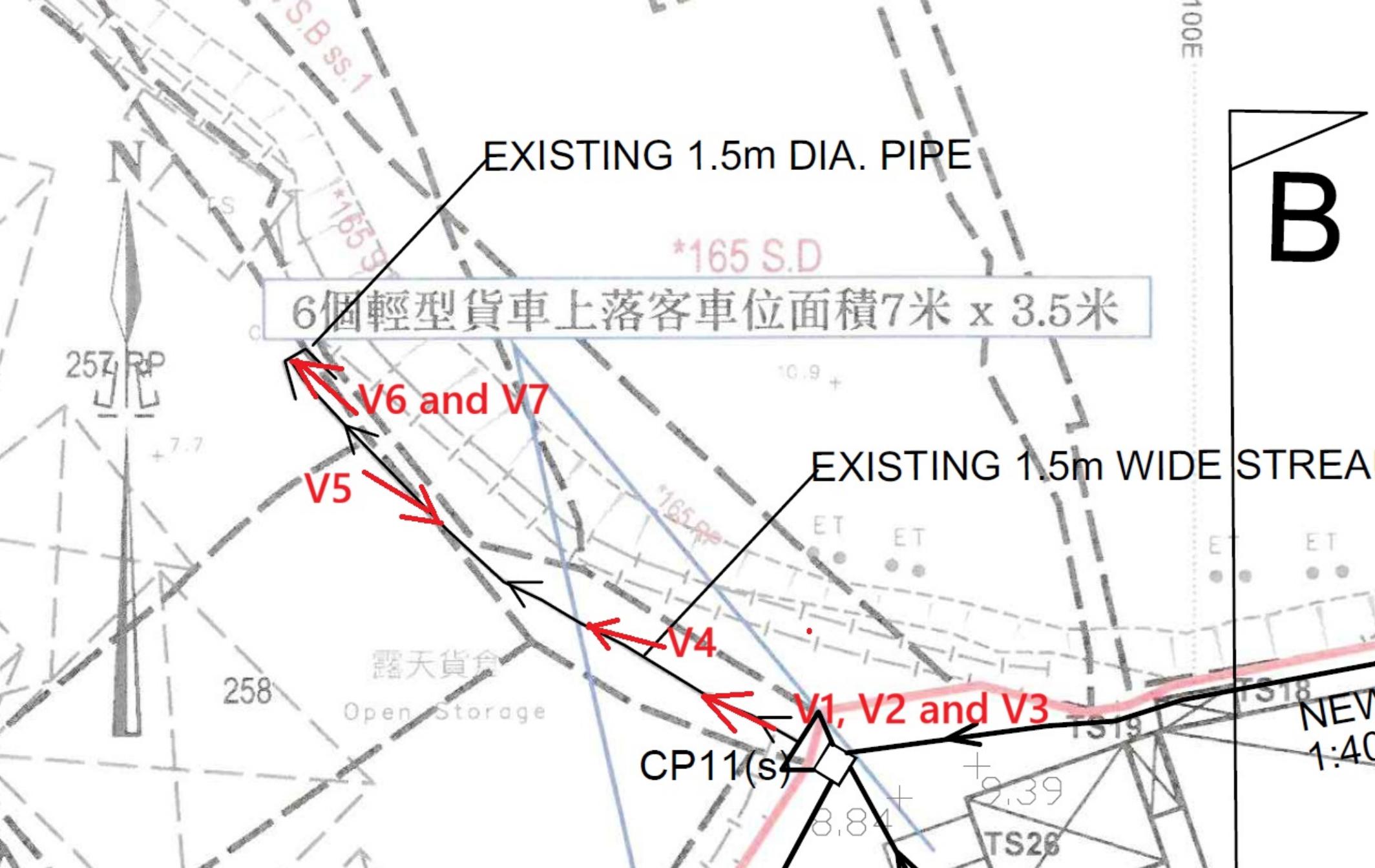


Figure 4d – Intensity-Duration-Frequency Curves of North District Area  
(for durations not exceeding 4 hours)

## **Appendix C**

### **Photo of Existing Stream and 1.5m Dia. Pipe**



EXISTING 1.5m DIA. PIPE

\*165 S.D

6個輕型貨車上落客車位面積7米 x 3.5米

V6 and V7

V5

EXISTING 1.5m WIDE STREAM

V4

V1, V2 and V3

CP11(s)

B

N

100E

257 RP

258

露天貨倉  
Open Storage

8.84

9.39

TS26

TS19

TS18

NEW  
1:40



**Photo no. V1 : General View of the Stream**



**Photo no. V2 : The Dimension of the Stream**



**Photo no. V3 : The Depth of the Stream**



**Photo no. V4 : General View of the Stream**



**Photo no. V5 : General View of the Stream**



**Photo no. V6 : General View of the 1.5m Dia. Pipe**



**Photo no. V7 : Dimension of the 1.5m Dia. Pipe**